

**Claim Amendments**

1. (currently amended) A method, a sensor array that employs a parameter to induce a time-varying phase angle  $\phi$  on an optical signal that comprises a phase generated carrier with a demodulation phase offset  $\beta$ , the method comprising the step of:

calculating the phase angle  $\phi$  substantially independently of the demodulation phase offset  $\beta$ .

2. (currently amended) The method of claim 1, further comprising the step of:

sampling an output signal from the sensor array to obtain a plurality of samples  $S_n$ , wherein  $n = 0$  to  $x$ ;

wherein the step of calculating the phase angle  $\phi$  substantially independently of the demodulation phase offset  $\beta$  comprises the step of:

calculating the phase angle  $\phi$  substantially independently of the demodulation phase offset  $\beta$  through employment of one or more of the plurality of samples  $S_n$ .

3. (currently amended) The method of claim ~~1~~ 2, wherein the step of calculating the phase angle  $\phi$  substantially independently of the demodulation phase offset  $\beta$  through employment of the one or more of the plurality of samples  $S_n$  comprises the steps of:

calculating one or more quadrature terms and one or more in-phase terms through employment of one or more of the plurality of samples  $S_n$ , wherein one or more of the one or more quadrature terms and one or more of the one or more in-phase terms are substantially independent from the demodulation phase offset  $\beta$ ; and

calculating the phase angle  $\phi$  through employment of the one or more quadrature terms and the one or more in-phase terms.

4. (original) The method of claim 2, wherein the output signal comprises a period  $T_{\text{pulse}}$ , wherein the step of sampling the output signal from the sensor array to obtain the plurality of samples  $S_n$ , wherein  $n = 0$  to  $x$  comprises the step of:

sampling the output signal from the sensor array to obtain a plurality of samples  $S_n$  within a period  $T_s$ , wherein  $n = 0$  to  $x$ , wherein  $T_s$  is less than or equal to  $1.125 \times T_{\text{pulse}}$ .

5. (original) The method of claim 4, wherein  $T_s$  is less than or equal to  $T_{\text{pulse}}$ .

6. (currently amended) The method of claim 4, wherein the step of calculating the phase angle  $\phi$  substantially independently of the demodulation phase offset  $\beta$  through employment of the one or more of the plurality of samples  $S_n$  comprises the steps of:

calculating one or more quadrature terms and one or more in-phase terms through employment of one or more of the plurality of samples  $S_n$ , wherein one or more of the one or more quadrature terms and one or more of the one or more in-phase terms are substantially independent from the demodulation phase offset  $\beta$ ;

calculating the phase angle  $\phi$  through employment of the one or more quadrature terms and the one or more in-phase terms.

7. (original) The method of claim 6, wherein the step of calculating the one or more quadrature terms and the one or more in-phase terms through employment of the one or more of the plurality of samples  $S_n$ , wherein the one or more of the one or more quadrature terms and the one or more of the one or more in-phase terms are substantially independent from the demodulation phase offset  $\beta$  comprises the steps of:

calculating a set of quadrature terms  $Q_j$  and a set of in-phase terms  $I_k$  through employment of one or more of the plurality of samples  $S_n$ , wherein  $j = 0$  to  $y$ , wherein  $k = 0$  to  $z$ ;

calculating a quadrature term  $Q_{ab}$  from a largest term of absolute values of the set of quadrature terms  $Q_j$ ;

calculating a constant  $C_1$  and a constant  $C_2$ ;

calculating a quadrature term  $Q_s = C_1 \times \sqrt{\sum_{j=0}^y Q_j^2}$ , wherein  $Q_s$  is substantially independent from the demodulation phase offset  $\beta$ ; and

calculating an in-phase term  $I_s = C_2 \times \sqrt{\sum_{k=0}^z I_k^2}$ , wherein  $I_s$  is substantially independent from the demodulation phase offset  $\beta$ .

8. (original) The method of claim 7, wherein the step of calculating the constant  $C_1$  and the constant  $C_2$  comprises the step of:

calculating the constant  $C_1$  and the constant  $C_2$  such that an amplitude of the quadrature term  $Q_s$ , an amplitude of the quadrature term  $Q_{ab}$ , and an amplitude of the in-phase term  $I_s$  comprise a substantially same amplitude for a modulation depth  $M$  of an operating range for the phase generated carrier.

9. (original) The method of claim 7, wherein  $x = 7$ ,  $y = 3$ ,  $z = 1$ , wherein the step of calculating the set of quadrature terms  $Q_j$  and the set of in-phase terms  $I_k$  through employment of the one or more of the plurality of samples  $S_n$ , wherein  $j = 0$  to  $y$ , wherein  $k = 0$  to  $z$  comprises the steps of:

calculating  $Q_0 = S_0 - S_4$ ;

calculating  $Q_1 = S_1 - S_5$ ;

calculating  $Q_2 = S_2 - S_6$ ;

calculating  $Q_3 = S_3 - S_7$ ;

calculating  $I_0 = (S_0 + S_4) - (S_2 + S_6)$ ; and

calculating  $I_1 = (S_1 + S_5) - (S_3 + S_7)$ .

10. (original) The method of claim 7, wherein  $x = 15$ ,  $y = 7$ ,  $z = 3$ , wherein the step of calculating the set of quadrature terms  $Q_j$  and the set of in-phase terms  $I_k$  through employment of the one or more of the plurality of samples  $S_n$ , wherein  $j = 0$  to  $y$ , wherein  $k = 0$  to  $z$  comprises the steps of:

calculating  $Q_0 = S_0 - S_8$ ;

calculating  $Q_1 = S_1 - S_9$ ;

calculating  $Q_2 = S_2 - S_{10}$ ;

calculating  $Q_3 = S_3 - S_{11}$ ;

calculating  $Q_4 = S_4 - S_{12}$ ;

calculating  $Q_5 = S_5 - S_{13}$ ;

calculating  $Q_6 = S_6 - S_{14}$ ;

calculating  $Q_7 = S_7 - S_{15}$ ;

calculating  $I_0 = (S_0 + S_8) - (S_4 + S_{12})$ ;

calculating  $I_1 = (S_1 + S_9) - (S_5 + S_{13})$ ;

calculating  $I_2 = (S_2 + S_{10}) - (S_6 + S_{14})$ ; and

calculating  $I_3 = (S_3 + S_{11}) - (S_7 + S_{15})$ .

11. (original) The method of claim 7, wherein the step of calculating the phase angle  $\phi$  through employment of the one or more quadrature terms and the one or more in-phase terms comprises the steps of:

calculating a correction term  $\Delta Q$ ;

calculating a quadrature term  $Q_m$  from the quadrature term  $Q_s$  and the correction term  $\Delta Q$ ;

calculating a quadrature term  $Q$  from a magnitude of the quadrature term  $Q_m$  and one or more quadrature terms of the set of quadrature terms  $Q_j$ ;

calculating an in-phase term  $I$  from a magnitude of the in-phase term  $I_s$  and one or more in-phase terms of the set of in-phase terms  $I_k$ ; and

calculating the phase angle  $\phi$  from an arctangent of a quantity  $Q / I$ .

12. (original) The method of claim 11, wherein the step of calculating the correction term  $\Delta Q$  comprises the step of:

calculating the correction term  $\Delta Q = Q_s - Q_{ab}$ .

13. (currently amended) The method of claim 11, wherein the step of calculating the quadrature term  $Q_m$  from the quadrature term terms  $Q_s$  and the correction term  $\Delta Q$  comprises the step of:

calculating a constant  $C_3$ ; and

calculating  $Q_m = Q_s + (C_3 \times \Delta Q)$ .

14. (currently amended) An apparatus, a sensor array that employs a parameter to induce a time-varying phase angle  $\phi$  on an optical signal that comprises a phase generated carrier with a demodulation phase offset  $\beta$ , the apparatus comprising:

a processor component that calculates the phase angle  $\phi$  substantially independent from the demodulation phase offset  $\beta$ .

15. (currently amended) The apparatus of claim 14, wherein the processor component obtains a plurality of samples  $S_n$  of an output signal from the sensor array, wherein  $n = 0$  to  $x$ ;

wherein the processor component employs one or more of the plurality of samples  $S_n$  to calculate the phase angle  $\phi$  substantially independent from the demodulation phase offset  $\beta$ .

16. (original) The apparatus of claim 15, wherein the processor component employs one or more of the plurality of samples  $S_n$  of the output signal to calculate one or more quadrature terms and one or more in-phase terms, wherein one or more of the one or more quadrature terms and one or more of the one or more in-phase terms are substantially independent from the demodulation phase offset  $\beta$  of the phase generated carrier;

wherein the processor component employs the one or more quadrature terms and the one or more in-phase terms to calculate the phase angle  $\phi$ .

17. (original) The apparatus of claim 15, wherein the output signal comprises a period  $T_{\text{pulse}}$ , wherein the processor component obtains the plurality of samples  $S_n$  within a period  $T_s$ , wherein  $T_s$  is less than or equal to  $1.125 \times T_{\text{pulse}}$ .



18. (original) The apparatus of claim 17, wherein  $T_s$  is less than or equal to  $T_{pulse}$ .

19. (original) The apparatus of claim 17, wherein the processor component employs one or more of the plurality of samples  $S_n$  of the output signal to calculate one or more quadrature terms and one or more in-phase terms, wherein one or more of the one or more quadrature terms and one or more of the one or more in-phase terms are substantially independent from the demodulation phase offset  $\beta$  of the phase generated carrier;

wherein the processor component employs the one or more quadrature terms and the one or more in-phase terms to calculate the phase angle  $\phi$ .

20. (original) The apparatus of claim 19, wherein the one or more of the one or more quadrature terms comprise a quadrature term  $Q_{ab}$  and a quadrature term  $Q_s$ , wherein the one or more of the one or more in-phase terms comprise an in-phase term  $I_s$ ;

wherein the processor component employs one or more of the plurality of samples  $S_n$ , the quadrature term  $Q_{ab}$ , the quadrature term  $Q_s$ , and the in-phase term  $I_s$  to calculate the phase angle  $\phi$ .

21. (original) The apparatus of claim 20, wherein the processor component employs the plurality of samples  $S_n$  to calculate a set of quadrature terms  $Q_j$  and a set of in-phase terms  $I_k$ , wherein  $j = 0$  to  $y$ , wherein  $k = 0$  to  $z$ ;

wherein the processor component employs the set of quadrature terms  $Q_j$  to calculate the quadrature term  $Q_{ab} = \max(|Q_j|)$ , wherein  $j = 0$  to  $y$ ;

wherein the processor component employs the set of quadrature terms  $Q_j$  and the set of in-phase terms  $I_k$  to calculate the quadrature term  $Q_s$ , and the in-phase term  $I_s$ .

22. (original) The apparatus of claim 21, wherein the processor component calculates a constant  $C_1$  and a constant  $C_2$ , wherein the processor component calculates:

$$Q_s = C_1 \times \sqrt{\sum_{j=0}^{j=y} Q_j^2};$$

wherein the processor component calculates:

$$I_s = C_2 \times \sqrt{\sum_{k=0}^{k=z} I_k^2};$$

wherein the processor component calculates the constant  $C_1$  and the constant  $C_2$  such that a magnitude of the quadrature term  $Q_s$ , a magnitude of the quadrature term  $Q_{ab}$ , and a magnitude of the in-phase term  $I_s$  comprise a substantially same magnitude at a modulation depth  $M$  of an operating range for the phase generated carrier.

23. (original) The apparatus of claim 22, wherein the processor component employs the quadrature term  $Q_{ab}$  and the quadrature term  $Q_s$  to calculate a correction term  $\Delta Q = Q_s - Q_{ab}$ ;

wherein the processor component employs the quadrature term  $Q_s$  and the correction term  $\Delta Q$  to calculate a quadrature term  $Q_m$ ;

wherein the processor component employs the quadrature term  $Q_m$ , the in-phase term  $I_s$ , the set of quadrature terms  $Q_j$ , and the set of in-phase terms  $I_k$  to calculate the phase angle  $\phi$ .

24. (original) The apparatus of claim 23, wherein the processor component employs the quadrature term  $Q_m$  and the set of quadrature terms  $Q_j$  to calculate a quadrature term  $Q$ , wherein the processor component employs the in-phase term  $I_s$  and the set of in-phase terms  $I_k$  to calculate an in-phase term  $I$ ;

wherein the processor component calculates:

$$Q = \pm Q_m;$$

wherein the processor component calculates:

$$I = \pm I_s;$$

wherein the processor component employs the set of quadrature terms  $Q_j$  to determine a sign of  $Q$ ;

wherein the processor component employs the set of in-phase terms  $I_k$  to determine a sign of  $I$ ;

wherein the processor component calculates:

$$\phi = \arctangent ( Q / I ).$$

25. (original) The apparatus of claim 24, wherein the processor component calculates a constant  $C_3$ , wherein the processor component calculates:

$$Q_m = Q_s + (C_3 \times \Delta Q).$$

26. (original) The apparatus of claim 25, wherein  $x = 7$ ,  $y = 3$ , and  $z = 1$ ;

wherein the processor component calculates:

$$Q_0 = S_0 - S_4, Q_1 = S_1 - S_5, Q_2 = S_2 - S_6, \text{ and } Q_3 = S_3 - S_7;$$

wherein the processor component calculates:

$$I_0 = (S_0 + S_4) - (S_2 + S_6); \text{ and}$$

$$I_1 = (S_1 + S_5) - (S_3 + S_7).$$

27. (original) The apparatus of claim 25, wherein  $x = 15$ ,  $y = 7$ , and  $z = 3$ ;

wherein the processor component calculates:

$$Q_0 = S_0 - S_8, Q_1 = S_1 - S_9, Q_2 = S_2 - S_{10}, Q_3 = S_3 - S_{11},$$

$$Q_4 = S_4 - S_{12}, Q_5 = S_5 - S_{13}, Q_6 = S_6 - S_{14}, \text{ and } Q_7 = S_7 - S_{15};$$

wherein the processor component calculates:

$$I_0 = (S_0 + S_8) - (S_4 + S_{12}), I_1 = (S_1 + S_9) - (S_5 + S_{13}),$$

$$I_2 = (S_2 + S_{10}) - (S_6 + S_{14}), \text{ and } I_3 = (S_3 + S_{11}) - (S_7 + S_{15}).$$

28. (currently amended) An article, a sensor array that employs a parameter to induce a time-varying phase angle  $\phi$  on an optical signal that comprises a phase generated carrier with a demodulation phase offset  $\beta$ , the article comprising:

one or more computer-readable signal-bearing media;

means in the one or more media for calculating the phase angle  $\phi$  substantially independently of the demodulation phase offset  $\beta$ .

29. (currently amended) The article of claim 28, further comprising:

means in the one or more media for sampling an output signal from the sensor array to obtain a plurality of samples  $S_n$ , wherein  $n = 0$  to  $x$ ;

wherein the means in the one or more media for calculating the phase angle  $\phi$  substantially independently of the demodulation phase offset  $\beta$  comprises:

means in the one or more media for calculating the phase angle  $\phi$  substantially independently of the demodulation phase offset  $\beta$  through employment of one or more of the plurality of samples  $S_n$ .

30. (currently amended) The article of claim 29, wherein the means in the one or more media for calculating the phase angle  $\phi$  substantially independently of the demodulation phase offset  $\beta$  through employment of the one or more of the plurality of samples  $S_n$  comprises:

means in the one or more media for calculating one or more quadrature terms and one or more in-phase terms through employment of one or more of the plurality of samples  $S_n$ , wherein one or more of the one or more quadrature terms and one or more of the one or more in-phase terms are substantially independent from the demodulation phase offset  $\beta$ ; and

means in the one or more media for calculating the phase angle  $\phi$  through employment of the one or more quadrature terms and the one or more in-phase terms.

31. (original) The article of claim 29, wherein the output signal comprises a period  $T_{\text{pulse}}$ , wherein the means in the one or more media for sampling the output signal from the sensor array to obtain the plurality of samples  $S_n$ , wherein  $n = 0$  to  $x$  comprises:

means in the one or more media for sampling the output signal from the sensor array to obtain the plurality of samples  $S_n$  within a period  $T_s$ , wherein  $n = 0$  to  $x$ , wherein  $T_s$  is less than or equal to  $1.125 \times T_{\text{pulse}}$ .

32. (original) The article of claim 31, wherein  $T_s$  is less than or equal to  $T_{pulse}$ .

33. (currently amended) The article of claim 31, wherein the means in the one or more media for calculating the phase angle  $\phi$  substantially independently of the demodulation phase offset  $\beta$  through employment of the one or more of the plurality of samples  $S_n$  comprises:

means in the one or more media for calculating one or more quadrature terms and one or more in-phase terms through employment of one or more of the plurality of samples  $S_n$ , wherein one or more of the one or more quadrature terms and one or more of the one or more in-phase terms are substantially independent from the demodulation phase offset  $\beta$ ;

means in the one or more media for calculating the phase angle  $\phi$  through employment of the one or more quadrature terms and the one or more in-phase terms.

34. (new) The article of claim 33, wherein the means in the one or more media for calculating the one or more quadrature terms and the one or more in-phase terms through employment of the one or more of the plurality of samples  $S_n$  comprises:

means in the one or more media for calculating a set of quadrature terms  $Q_j$  and a set of in-phase terms  $I_k$  through employment of one or more of the plurality of samples  $S_n$ , wherein  $j = 0$  to  $y$ , wherein  $k = 0$  to  $z$ ;

means in the one or more media for calculating a quadrature term  $Q_{ab}$  from a largest term of absolute values of the set of quadrature terms  $Q_j$ ;

means in the one or more media for calculating a constant  $C_1$  and a constant  $C_2$ ;

means in the one or more media for calculating a quadrature term  $Q_s = C_1 \times \sqrt{\sum_{j=0}^{j=y} Q_j^2}$ ,

wherein  $Q_s$  is substantially independent from the demodulation phase offset  $\beta$ ; and

means in the one or more media for calculating an in-phase term  $I_s = C_2 \times \sqrt{\sum_{k=0}^{k=z} I_k^2}$ ,

wherein  $I_s$  is substantially independent from the demodulation phase offset  $\beta$ .

35. (new) The article of claim 34, wherein the means in the one or more media for calculating the constant  $C_1$  and the constant  $C_2$  comprises:

means in the one or more media for calculating the constant  $C_1$  and the constant  $C_2$  such that an amplitude of the quadrature term  $Q_s$ , an amplitude of the quadrature term  $Q_{ab}$ , and an amplitude of the in-phase term  $I_s$  comprise a substantially same amplitude for a modulation depth  $M$  of an operating range for the phase generated carrier.



36. (new) The article of claim 34, wherein the means in the one or more media for calculating the phase angle  $\phi$  through employment of the one or more quadrature terms and the one or more in-phase terms comprises:

means in the one or more media for calculating a correction term  $\Delta Q$ ;

means in the one or more media for calculating a quadrature term  $Q_m$  from the quadrature term  $Q_s$  and the correction term  $\Delta Q$ ;

means in the one or more media for calculating a quadrature term  $Q$  from a magnitude of the quadrature term  $Q_m$  and one or more quadrature terms of the set of quadrature terms  $Q_j$ ;

means in the one or more media for calculating an in-phase term  $I$  from a magnitude of the in-phase term  $I_s$  and one or more in-phase terms of the set of in-phase terms  $I_k$ ; and

means in the one or more media for calculating the phase angle  $\phi$  from an arctangent of a quantity  $Q / I$ .

37. (new) The article of claim 34, wherein the means in the one or more media for calculating the correction term  $\Delta Q$  comprises:

means in the one or more media for calculating the correction term  $\Delta Q = Q_s - Q_{ab}$ ;

wherein the means in the one or more media for calculating the quadrature term  $Q_m$  from the quadrature term  $Q_s$  and the correction term  $\Delta Q$  comprises:

means in the one or more media for calculating a constant  $C_3$ ; and

means in the one or more media for calculating  $Q_m = Q_s + (C_3 \times \Delta Q)$ .